



**SWTEST**

PROBE TODAY, FOR TOMORROW

**2022 CONFERENCE**

# Challenges of Magnetic Field Probe Cards



Jory Twitchell/Jansen  
Currens  
NXP Semiconductor



Brandon Mair  
Technoprobe America Inc.

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# Presentation Overview

- Background for magnetic field probe card presentations at SW Test
- Probe card requirements
- Wafer prober chuck simulation
- Simulation of magnetic fields
- Challenges to overcome
- Summary of production results
- Questions?
- Answers!!!

# Magnetic Field Probe Cards

- **Multi-site probing of magnetic sensors at 175 deg C – Melexis/JEM**
  - Presented SW Test 2016
  - [http://www.swtest.org/swtw\\_library/2016proc/PDF/S07\\_01\\_Gouwy\\_SWTW2016.pdf](http://www.swtest.org/swtw_library/2016proc/PDF/S07_01_Gouwy_SWTW2016.pdf)
- **Sensors at Test – “Magnetic” Probe Cards – T.I.P.S. Messtechnik GmbH/TI**
  - Presented SW Test 2017
  - [https://www.swtest.org/swtw\\_library/2017proc/PDF/T01\\_01\\_Gaggl\\_SWTW2017.pdf](https://www.swtest.org/swtw_library/2017proc/PDF/T01_01_Gaggl_SWTW2017.pdf)
- **3D Magnetic sensor simulation - T.I.P.S. Messtechnik GmbH**
  - Presented at SW Test 2021
  - [https://www.swtest.org/swtw\\_library/2021proc/pdf/od\\_02\\_franz\\_swtest\\_2021.pdf](https://www.swtest.org/swtw_library/2021proc/pdf/od_02_franz_swtest_2021.pdf)
- **Simple explanation of magnetic field**
  - <https://www.youtube.com/watch?v=bq6lhpfucE>

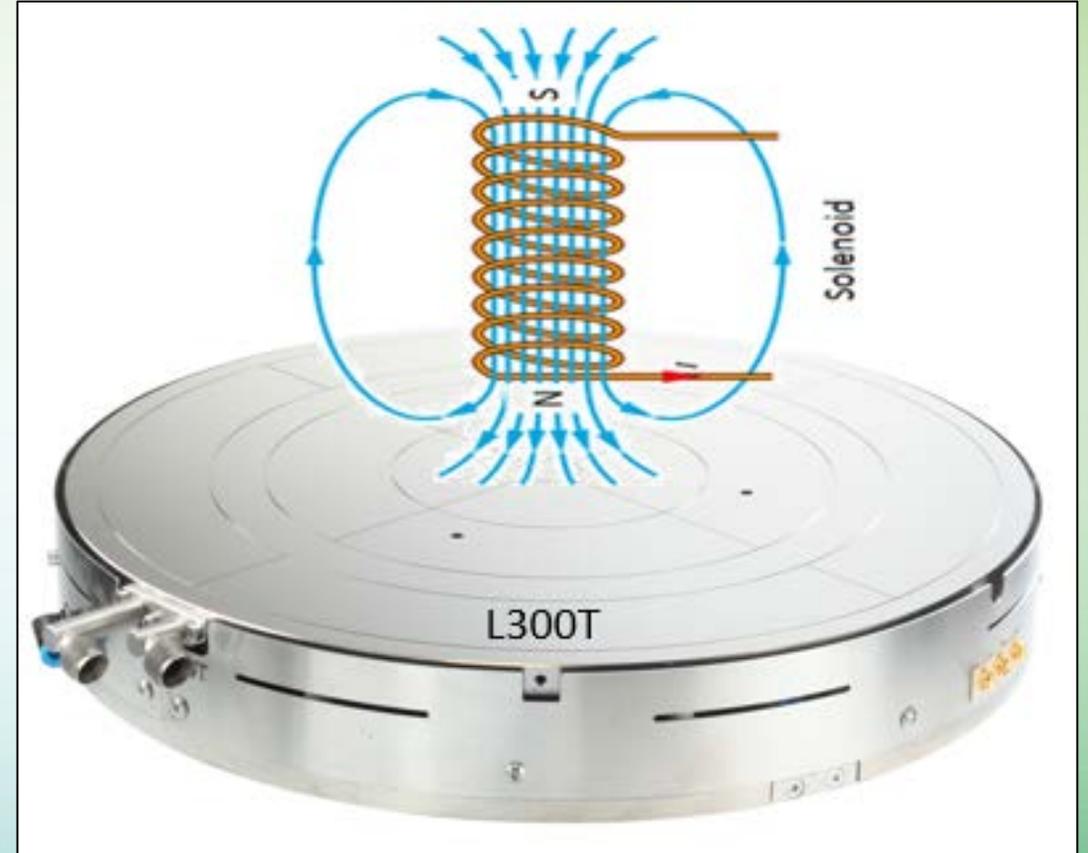
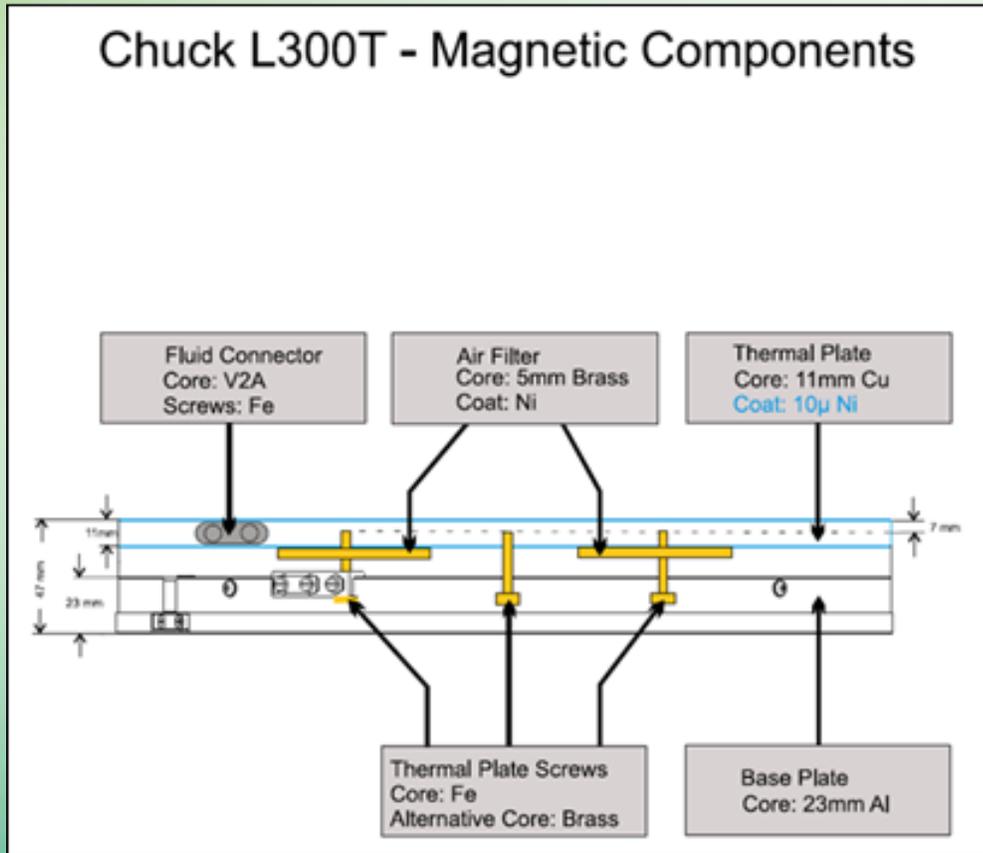
# Probe Card Requirements

- Design probe card for single Z-axis hall effect magnetic field sensor
- Product will be a small die with PDPW greater than 25K
- Parallelism 64 DUT's
- Advantest 93K test system which is standard production tester/prober setup
- Magnetic field target: 200 Gauss  $\pm 7$  Gauss
- Out-of-Plane, Hz
- Maximum distance of all hardware from bottom of PCB  $\leq 20$ mm
- Single Coil ("LARGE")
- Test Temperature: Room Temperature

# Chuck Simulation Plan

1. Hz on chuck surface  $\geq$  requirement spec?
  - Use simulation to determine coil size and appropriate chuck to coil distance
2. Hz already inaccurate due to background fields?
  - Chucks alone were measured at vendor
  - Chucks in prober were measured in NXP: For both “standard chuck” and “non-magnetic” chuck at 30°C
3. Magnetization of chuck components by strong Hz field?
  - Vendor provided a drawing/sketch about the “standard-chuck” top layers
  - Simulate (top layers, w.r.t. DUT area, with magnetic properties), monitoring various components
  - All chuck components were found to be exposed to Hz fields  $\ll$  their corrective field strength
4. Hz sufficiently homogeneous over DUT area?
  - Initial thought: Field lines distorted into x- and y-direction when penetrating the chuck (might be even worse with TiN coating of non-magnetic chuck, which is intended for parallel field lines)
  - Use simulation for standard chuck and components: Hz variation within DUT area of  $\pm 2.3\%$
  - Experiment: Over chuck and driven with current; measure Hz vs. DUT area.

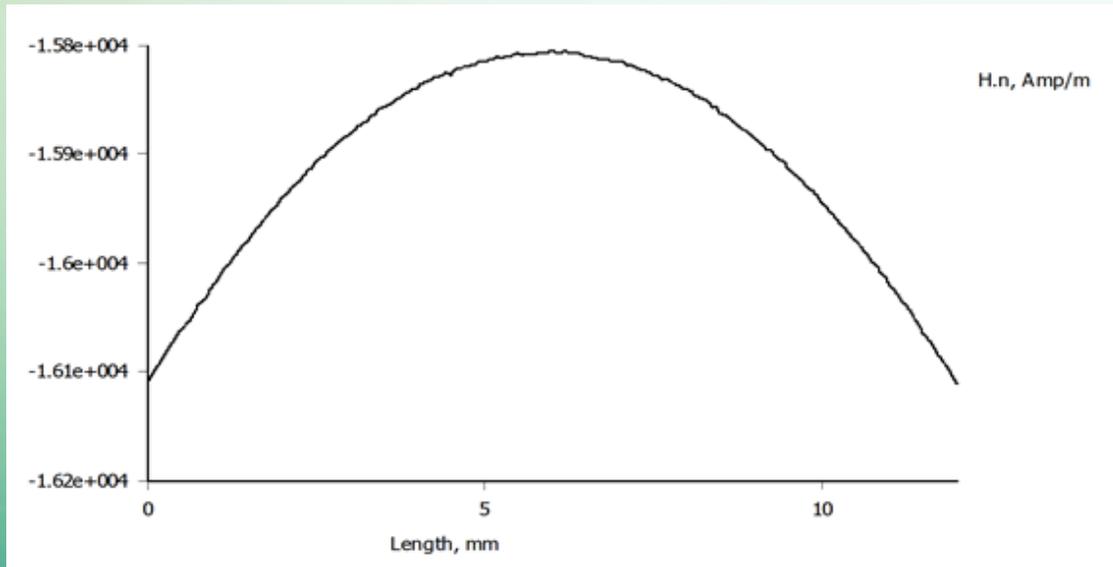
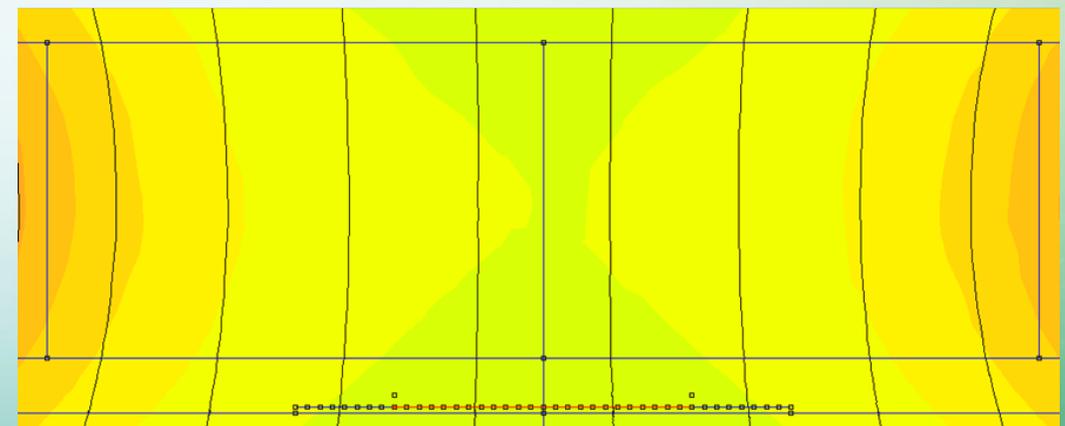
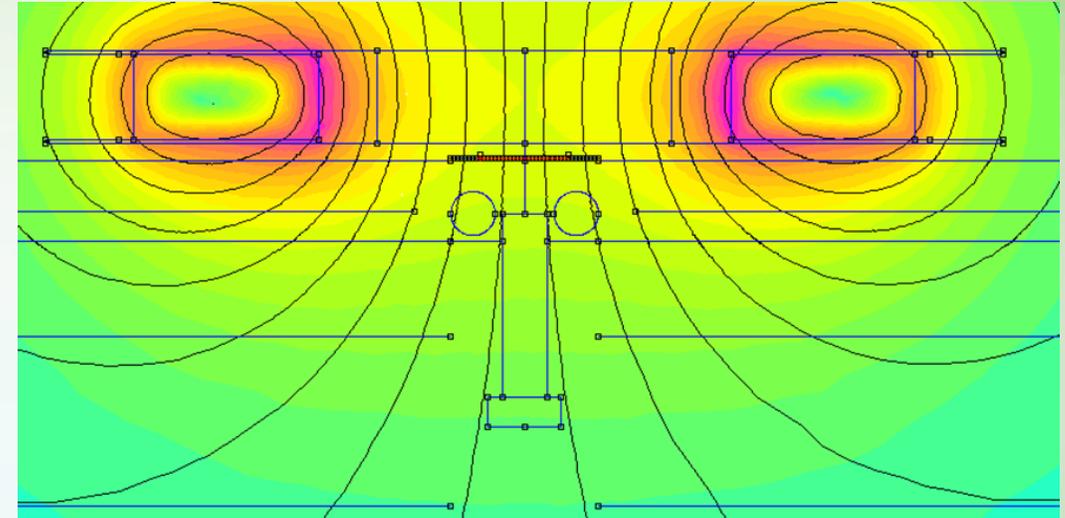
# Chuck Illustration



# L300T Chuck Simulation 1

## No Ferromagnetic Parts or Coatings

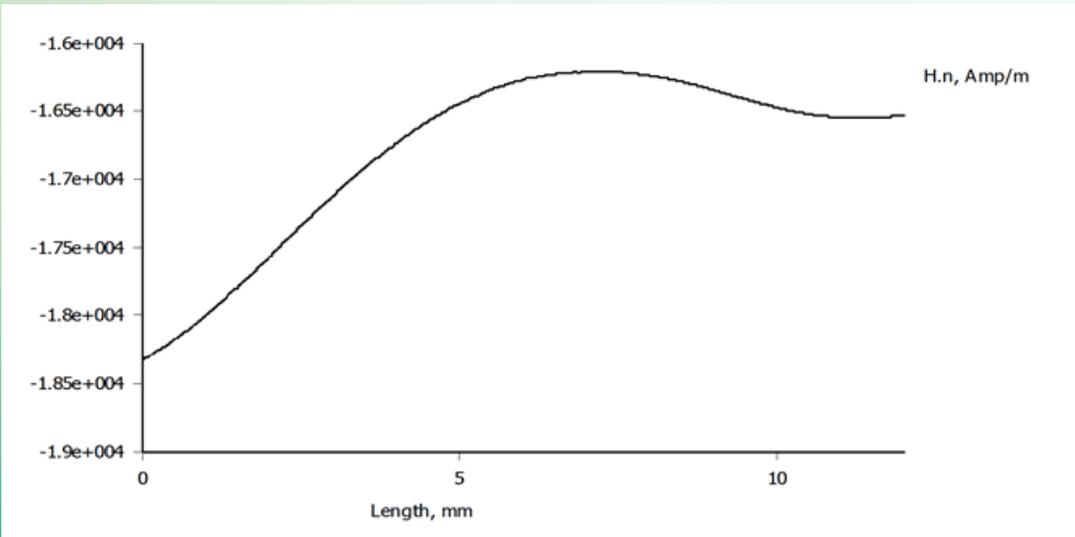
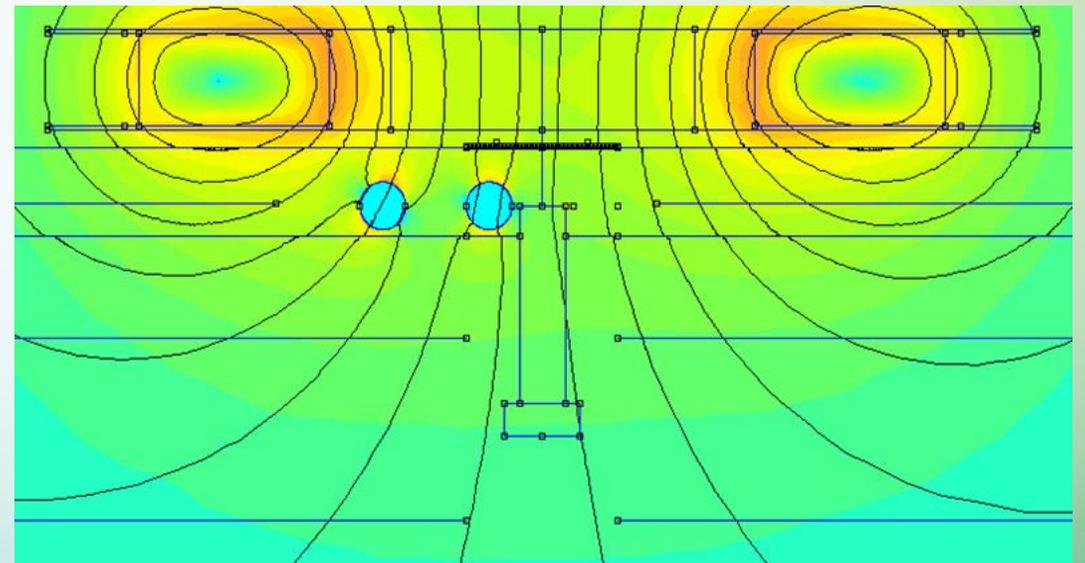
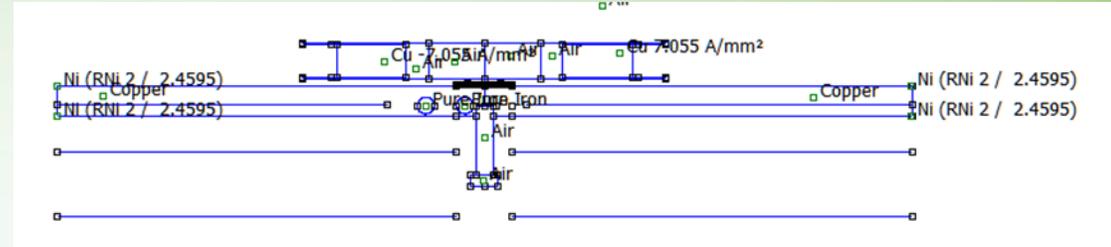
- 2D simulation in cross-cut view
- Readings for showing basic effects only!
- Red dotted line indicates DUT area
- $H_{dut} = 15948.2 \text{ A/m}$  ( $200.4 \text{ G}$ )  $\pm 0.9\%$



# L300T Chuck Simulation 6

## Shifted Ferromagnetic Screws at Fluid Connector With Top & Bottom Ni Coating

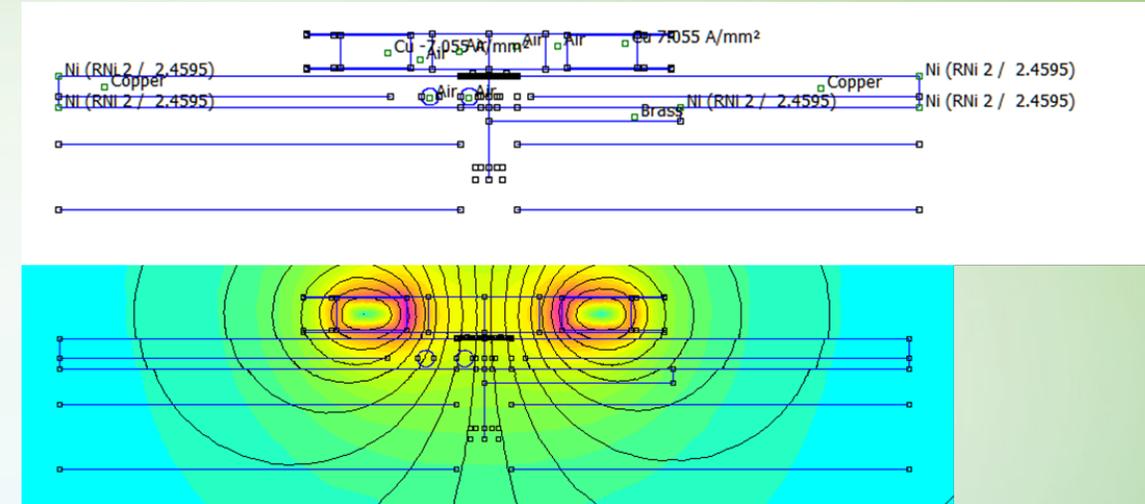
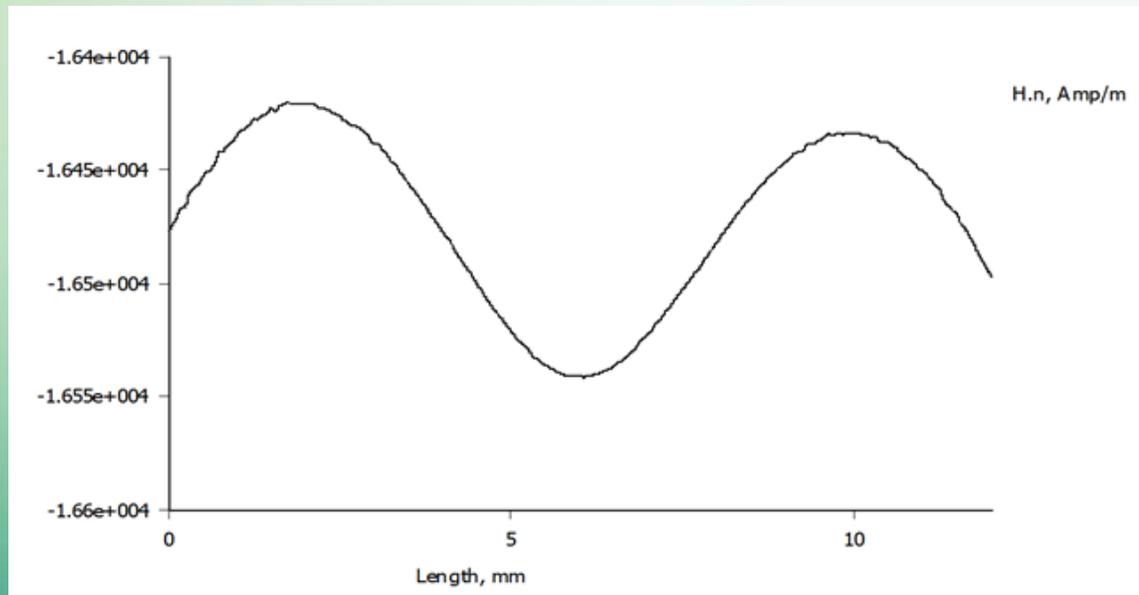
- 2D simulation in cross-cut view
- Readings for showing basic effects only!
- $H_{dut} = 18337\text{-}16264 \text{ A/m}$   
„linear“ (217.4 G)  $\pm 6.0\%$



# L300T Chuck Simulation 7

## 5 $\mu$ Ni Coated Brass and Top & Bottom Coating

- 2D simulation in cross-cut view
- Readings for showing basic effects only!
- $H_{dut} = 16480 \text{ A/m}$  (207.1 G)  $\pm 0.37\%$



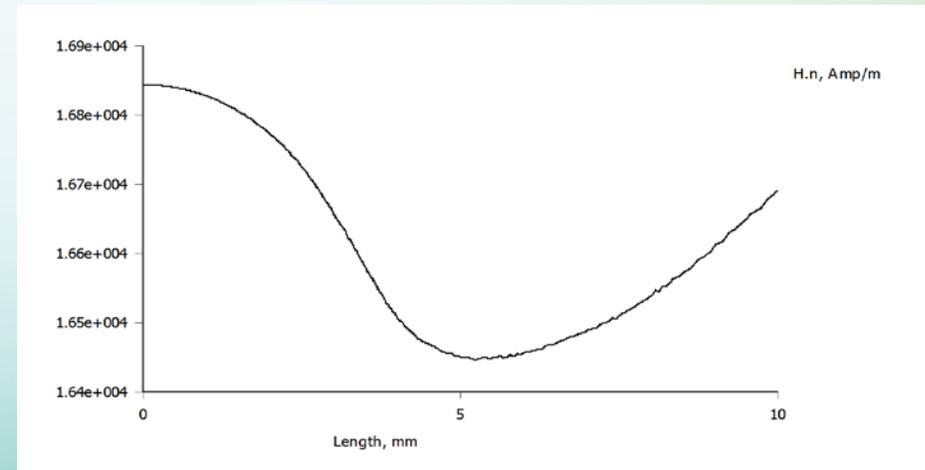
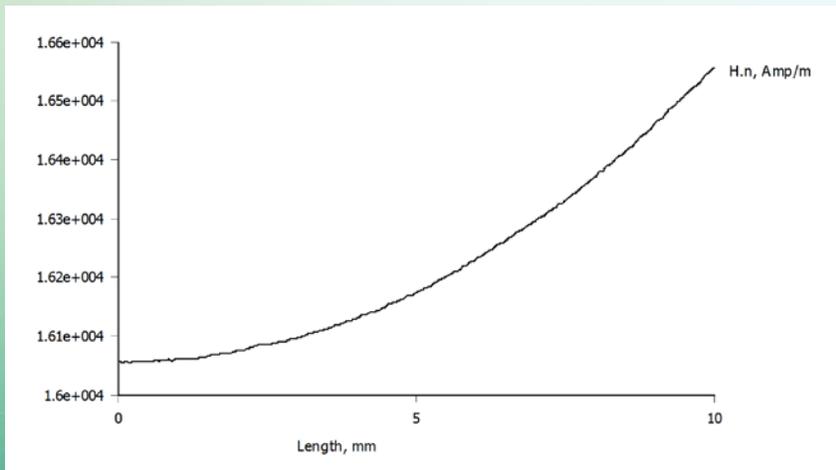
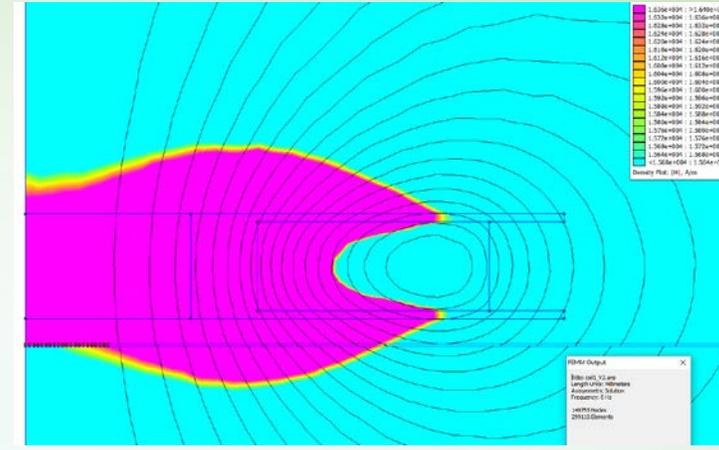
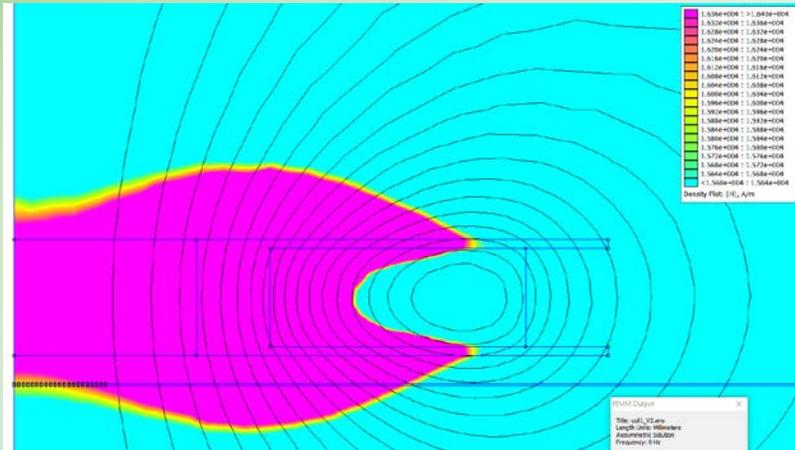
# L300T Chuck Simulation Summary

- Nickel coat on thermal plate does not hamper
- Nickel coated brass has minor impact
- Thermal plate screws have high impact on homogeneity
  - Recommendation: to be replaced by non ferro magnetic parts to reduce variation from  $\pm 2.3\%$  down to  $< 0.5\%$
- No magnetizing with remanence observed in simulations, all magnetization of the standard chuck screws is below coercivity force
- Air, Brass, Aluminum, V2A Steel, copper taken as magnetic inert,  $\mu_r=1$
- Calc:  $H_{dut} = (H_{max} + H_{min}) / 2$ ; Range:  $(H_{max} - H_{min}) / 2 / H_{dut}$

# Coil Design – 1<sup>st</sup> attempt

1. Z= 12.75mm
  2. Inside Diameter = 40mm
  3. Outside Diameter = 130mm
  4. 200 Gauss
  5. Resistance 900mΩ
  6. Temp @ 20% Duty Cycle -> 53C coil center in air
- **Pro's of this Coil design**
    - Meets requirements by production of overall height to be <= to 20 mm
    - Resistance is low
  - **Con's of this Coil design**
    - Need to maintain room temperature at DUT with no external input
      - This could be difficult to achieve with coil temperature at simulated 53°C
  - **Need simulation to verify coil design meets requirements**

# Coil Design 1 Simulation



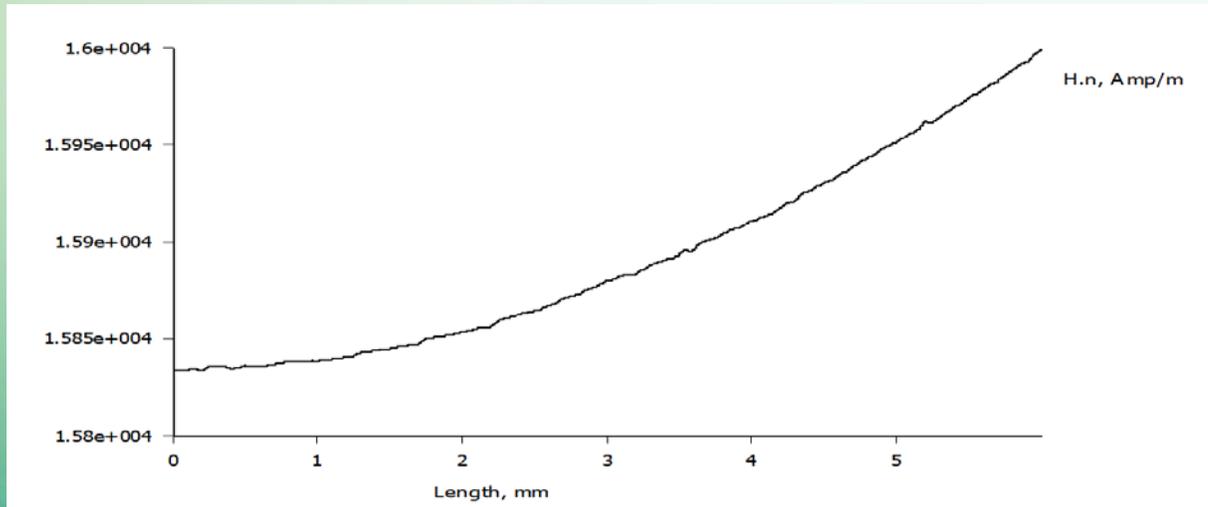
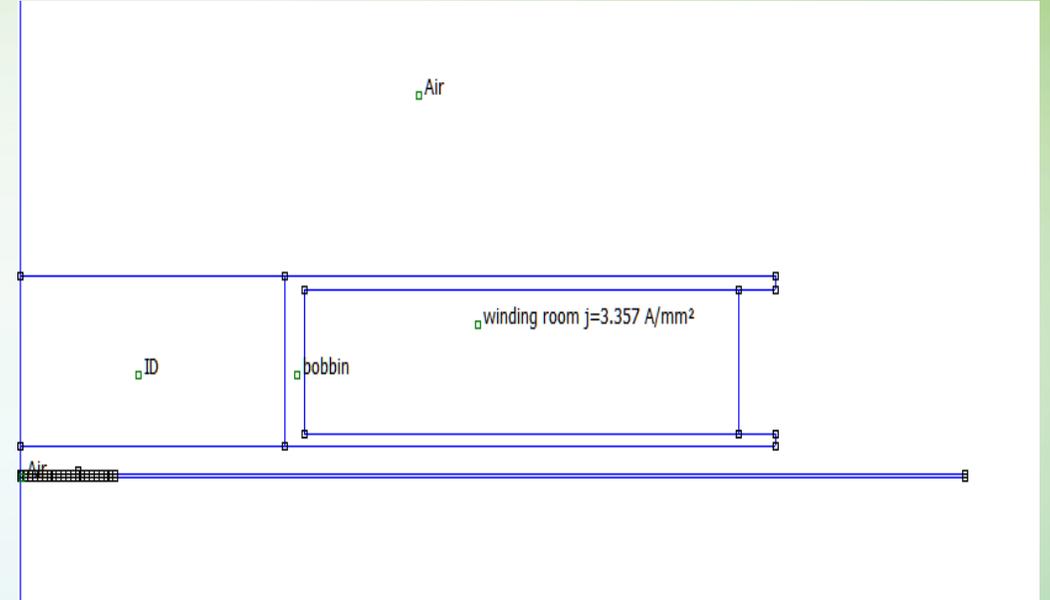
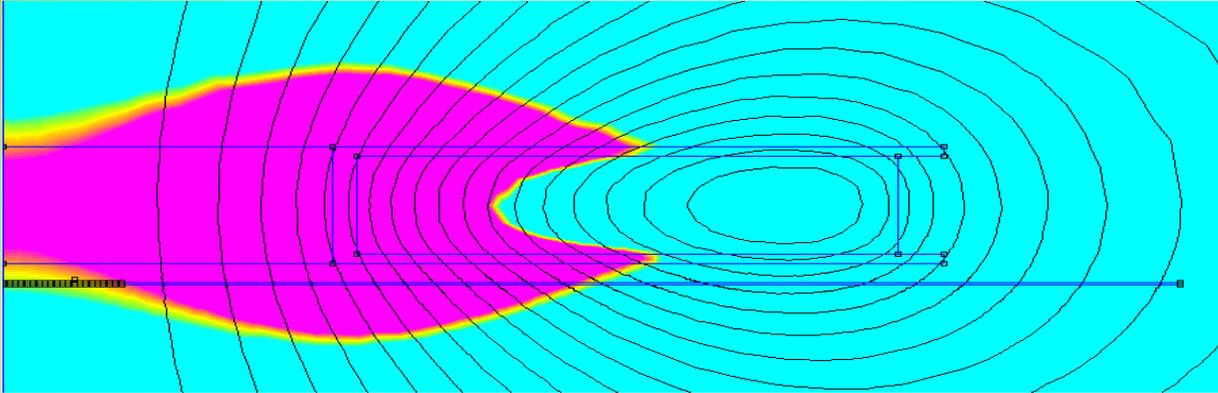
Without Mu-Metal

With Mu-Metal

# Coil Design Final Attempt

- The coil design and simulation process continued for 6 additional designs before concluding design 7 met all specifications
  1.  $Z = 12.5\text{mm} \pm 0.25\text{mm}$
  2. Inside Diameter = 56mm
  3. Outside Diameter = 160 mm
  4. 200 Gauss
  5. Resistance 470m $\Omega$
  6. Temp @ 20% Duty Cycle -> 52°C Coil center
- Changes from 1<sup>st</sup> design
  - Decrease Z
  - Increase inside and outside diameter
  - Lower resistance

# Coil Design Final Simulation



The radius of interest covered approximately 5mm. The accuracy in the area of interest was 200Gs +/- 0.53%.

# Challenges - Temperature

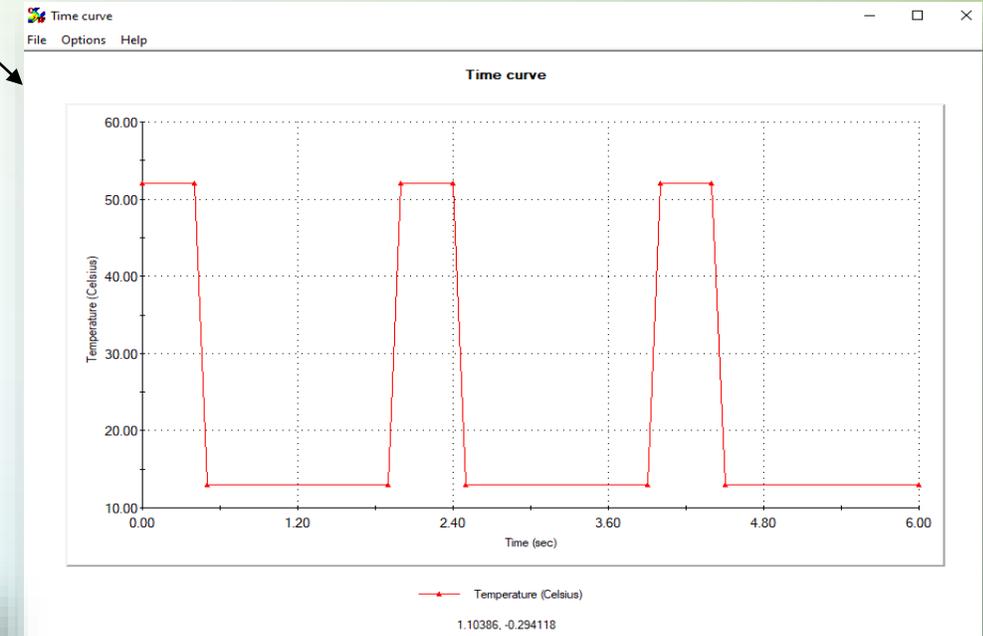
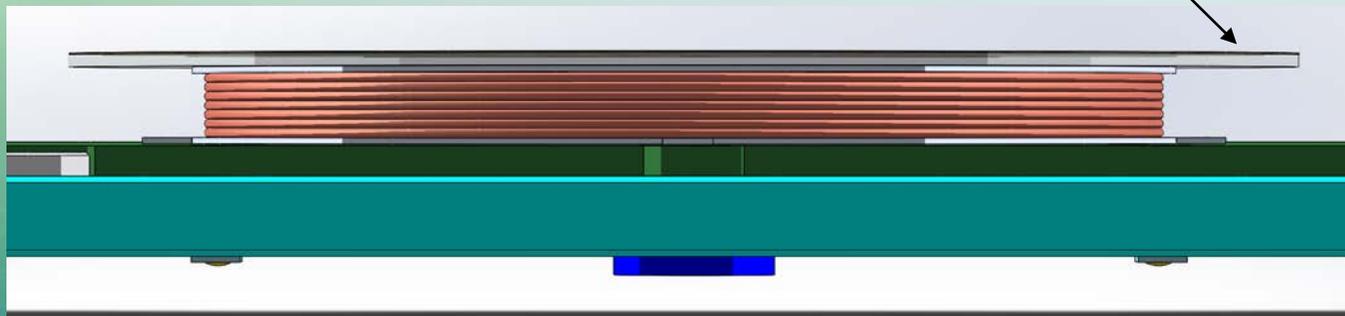
- The coil specifications complete - time to tackle the remaining challenges:
- Temperature of DUT required to stay at room temperature
- Coil temperature surrounding the DUT 52°C
- Need ways to reduce the temperature of the DUT to room temperature????
  - Thermal chuck
  - CDA (Clean Dry Air)
  - CDA through coil
- Would it work to use the PCB stiffener as a heat sink?

# Challenges - Temperature- Model

- Create the model specifications to perform simulation

Studying the thermal response of a wafer under a 52°C coil. 20% PWM under 2 seconds oscillation at the coil.

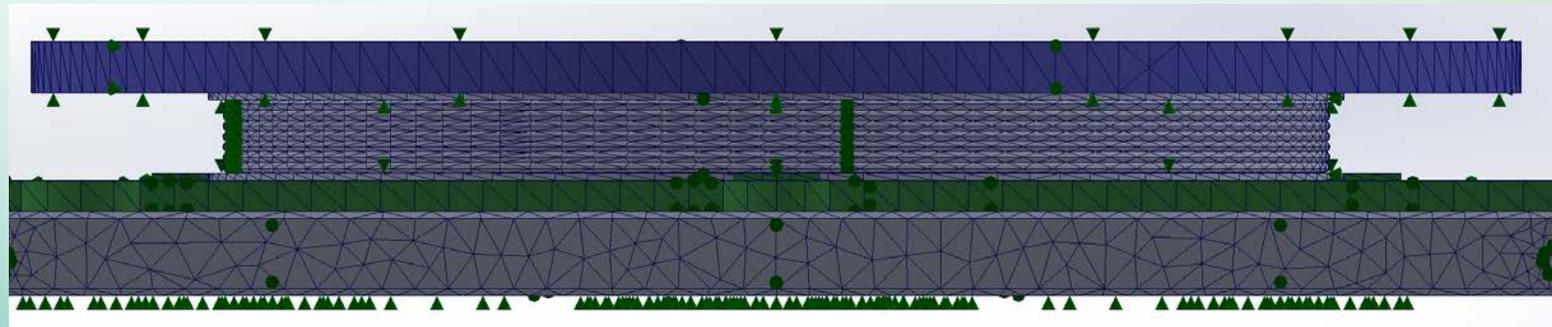
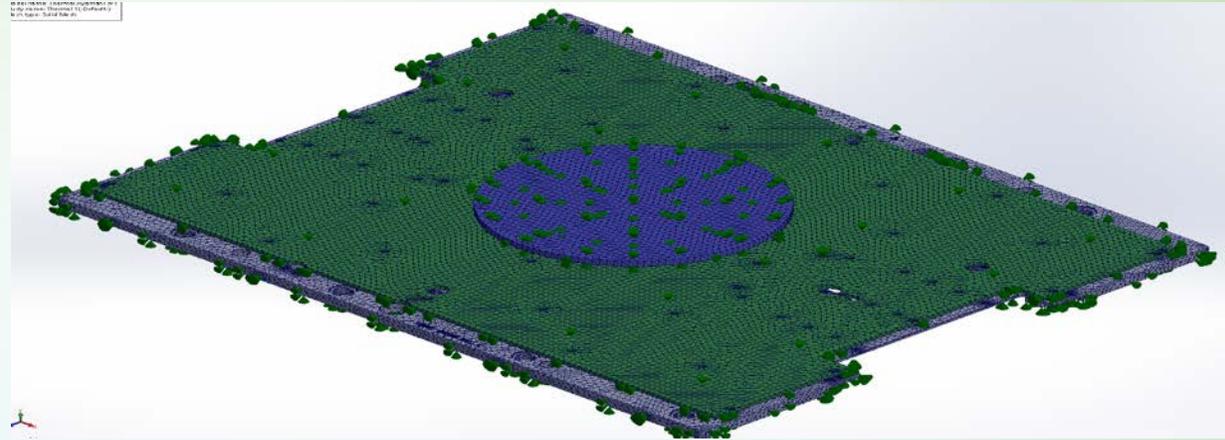
Air disk modeled, 2mm separation between wafer and coil.



# PCB and Coil Model

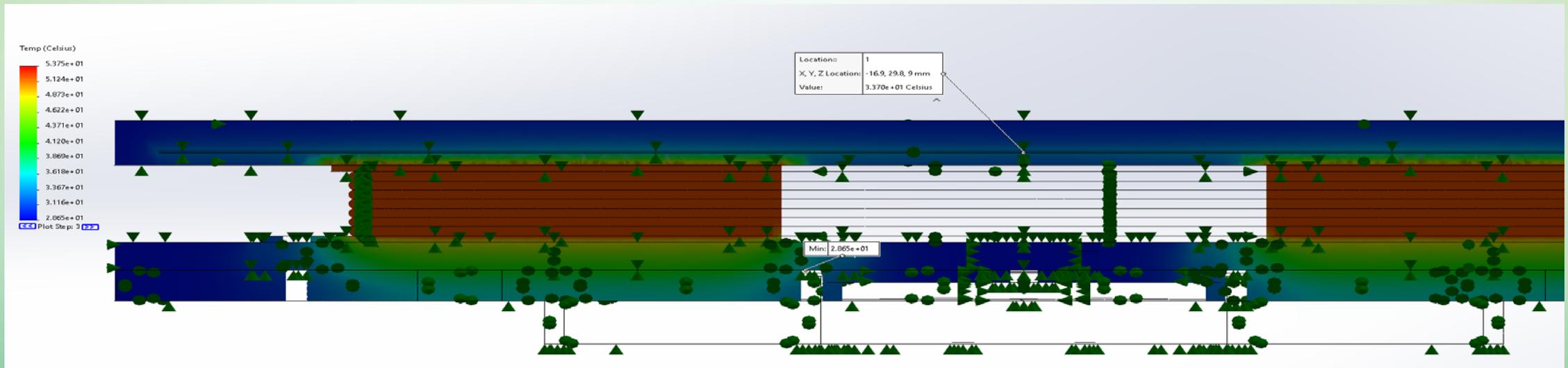
- Standard 5mm mid quality element refined mesh, with 0.25mm tolerance
- Mesh refinement at wafer and board
- 1,043,533 nodes
- 624,703 elements

The final mesh stack included the board, stiffener, and inlay plate.



# Challenges – Temperature Simulation

- 29°C ambient temp. Board, Stiffener, & inlay plate included. Increased copper pads for thermal dissipation added. Air volume unchanged from previous simulations.
- 33°C result in wafer, slight improvement from previous simulations
- Coil is heating evenly, small help from copper features



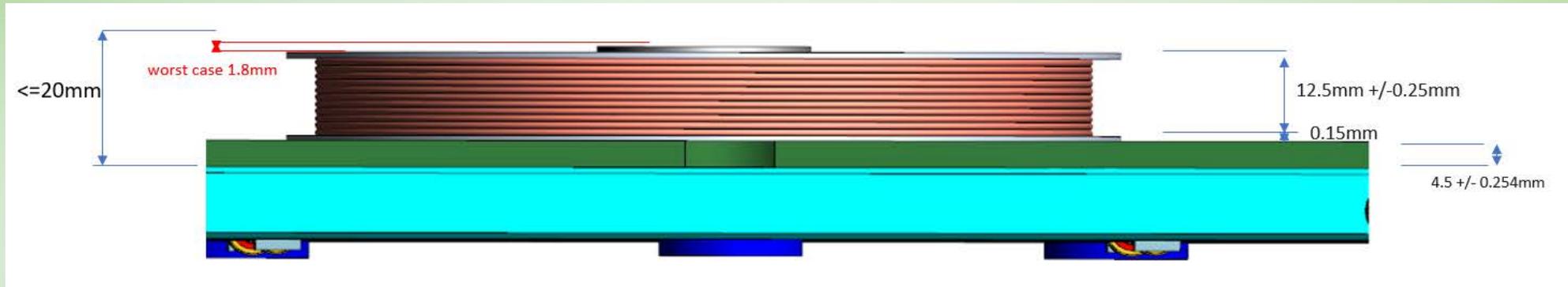
Conclusion: Despite the small improvement by adding the copper it is highly recommended to add copper or thermal relieves where possible

# Probe Card Design Challenges:

During the Probe Card Design. There were a couple challenges that had to be overcome.

1. Maximum distance of all hardware from bottom of PCB(PCB tester side)  $\leq 20\text{mm}$
2. Design of the thin copper layer  $150\mu\text{m}$  that goes between coil and PCB for heat dissipation continuity.

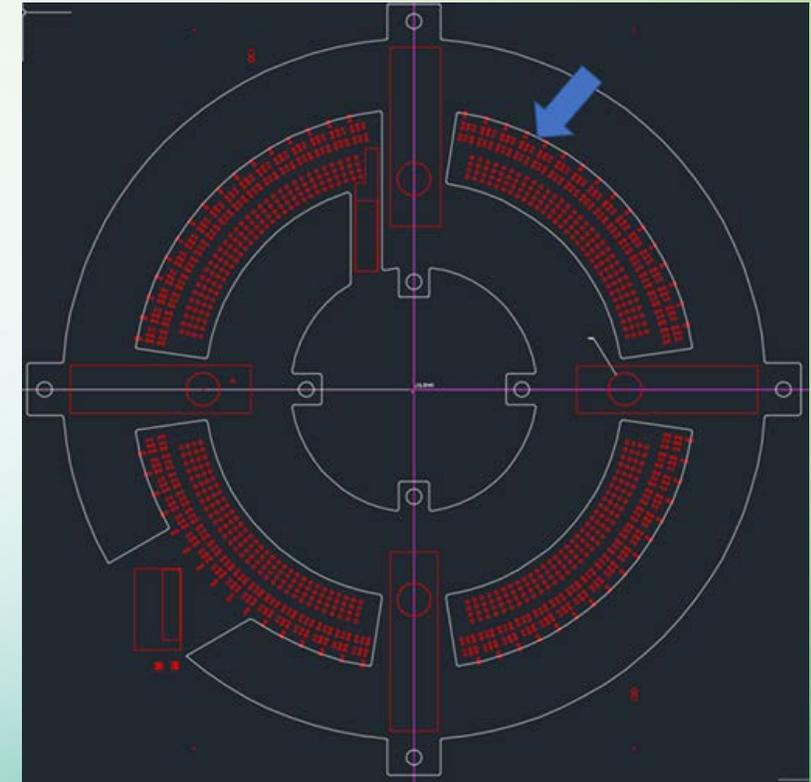
# Design Challenges: Max Clearance $\leq 20\text{mm}$



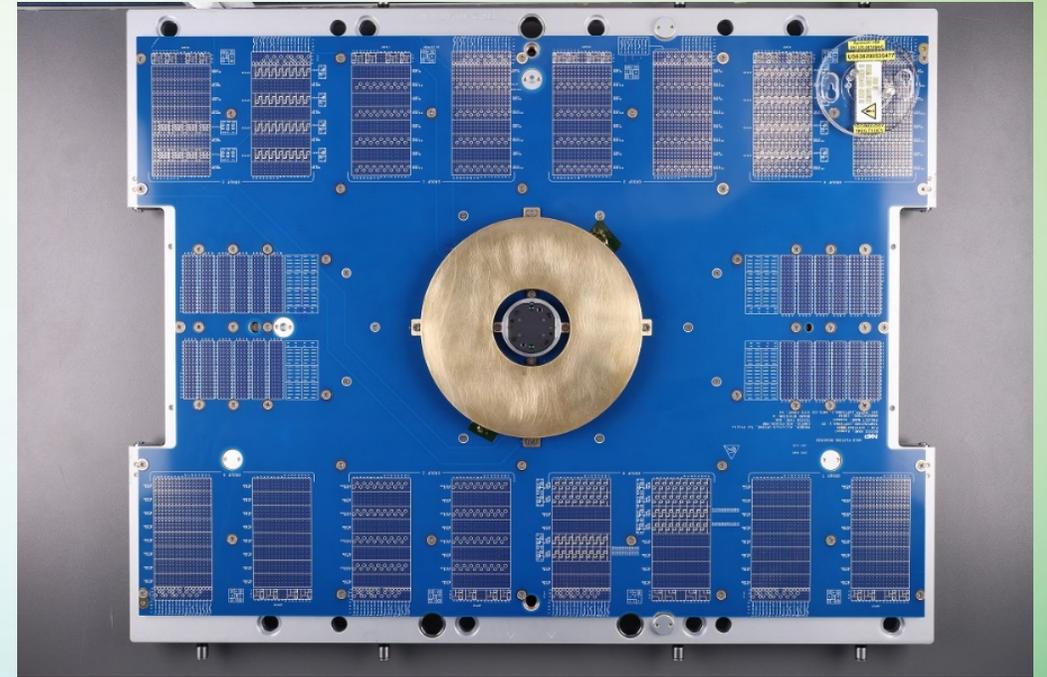
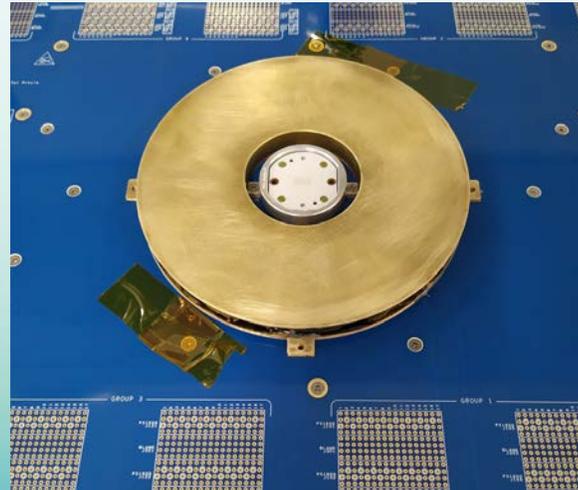
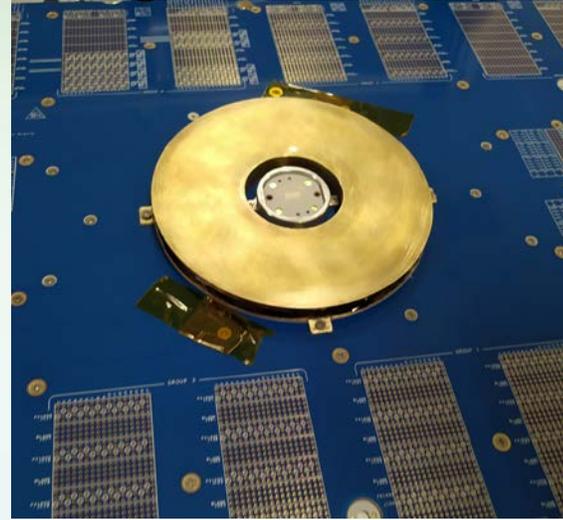
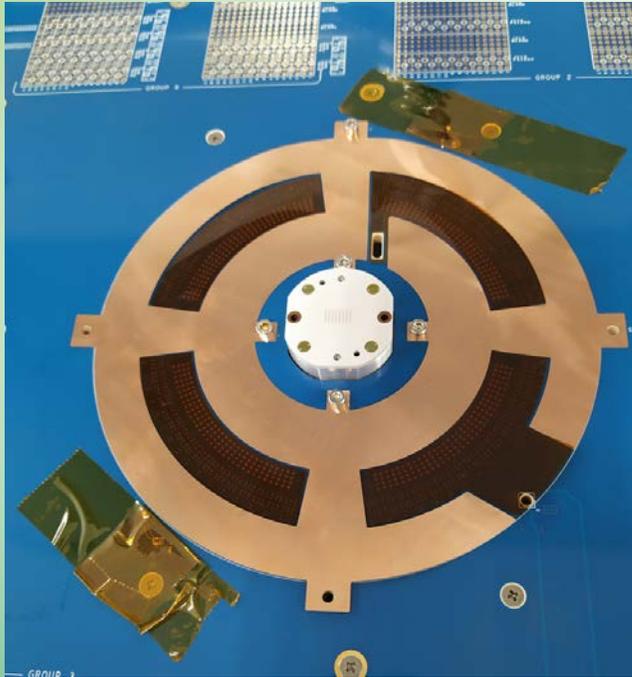
- Fix the Coil on PCB wafer side with small room between coil surface and needle tip (ideal target of 1.8mm but not below 1.5mm safety margin).
- Other suggestions:
  - Don't reduce furtherly the room between needle tip and coil surface
  - If coil thickness needs to increase, you can act by the below in order to keep safety margin unchanged:
    - Reducing PCB thickness
    - Increasing maximum distance acceptable from bottom PCB

# Design Challenge: Heat Dissipation

- Design of the thin copper layer 150um that goes between coil and PCB for heat dissipation continuity.
- Characteristic of the thin copper layer:
  - Compensate the different height between PCB surface and coil
  - Guarantee thermal continuity between heat dissipation pads on the PCB and coil cover
  - Avoid short between solder pads, components and the coil terminal pad



# Probe Card Photos



# Summary/Follow Up Work

- Summary from business line:
  - Yields are as expected on initial wafers processed
  - Final simulation data matches the actual wafer data for uniformity of magnetic field across the DUT array
  - Temperature measured on the die is consistent at 30°C
  
- Follow up work to be completed:
  - Production Probe Design of Experiment (PDOE) passes
  - Wafer Test to Final Test comparison - Was there any unexpected fallout
  - Monitor lifetime of probe card, coil

# Thank you

- NXP and TechnoProbe would like to thank the following people for their work in helping make this project a success

## NXP

- Weng Yap
- Joe Millazo
- Trent Cohrt
- Bary Turley
- Brian Nakai
- Engelbert Steffens
- Peter Löptien
- ATT Systems



## Technoprobe

- Andrea Motta
- Stefano Beretta
- Antonino Riolo
- Alessandro Albanetti

- We would also like to thank SW Test committee for allowing us to present on this topic

# Questions????

